

**APPLICATION FOR UNITED STATES PATENT**

**PROCESS FOR MINIMIZING AFTERBURN IN A FCC REGENERATOR**

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**CROSS-REFERENCE TO RELATED APPLICATIONS**

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## PROCESS FOR MINIMIZING AFTERBURN IN A FCC REGENERATOR

### CROSS-REFERENCE TO RELATED APPLICATIONS

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[0001] This patent application claims benefit of U.S. provisional patent application 60/213,911 filed June 26, 2000.

### BACKGROUND

10 [0002] The invention relates to a process and apparatus for controlling afterburning in the regenerator of a fluid catalytic cracking unit (FCCU).

[0003] Fluidized catalytic cracking (FCC) of conventional feeds may be accomplished by a variety of processes that employ fluidized solid techniques. Normally in such processes, the FCC feed contacts a cracking catalyst in a fluidized 15 bed reaction zone or in an riser reaction zone.

20 [0004] During the cracking reaction, coke deposits on the catalyst particles in the reaction zone, thereby reducing the activity of the catalyst for cracking. To restore the activity of the spent catalyst, the catalyst is transferred from the reaction zone into a regeneration zone. A regeneration zone may comprise a large vertical substantially cylindrical vessel wherein the spent catalyst is maintained as a fluidized bed by the upward passage of an oxygen-containing regeneration gas, preferably air. The fluidized catalyst forms a dense phase catalyst bed in the lower portion of the vessel and a dilute phase in the upper portion of the vessel. The 25 dilute phase contains entrained catalyst particles. The spent catalyst contacts the oxygen-containing regeneration gas under conditions sufficient to burn at least a portion of the coke from the catalyst. The flue gas exiting the regenerator comprises gases arising from the combustion of the coke on the spent catalyst, inert gases such as nitrogen from air, and unreacted oxygen. Before exiting the regenerator, the flue gas passes from the dilute phase into solid-gas separators

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within the regeneration zone (e.g., cyclone separators) to prevent excessive losses of the entrained catalyst particles. The catalyst particles separated from the flue gas return to the dense phase catalyst bed. The regenerated catalyst is subsequently recycled to the reaction zone.

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[0005] Regenerators typically operate under either full-burn conditions or partial-burn conditions. Under full-burn conditions, the regenerator is designed to operate so that substantially all of the carbon monoxide (CO) in the regenerator gases combusts to form carbon dioxide (CO<sub>2</sub>), thereby imparting the heat of reaction to the regeneration zone. Under partial-burn conditions, the regenerator is designed to operate so that only a portion of the CO combusts to CO<sub>2</sub>, the remainder of the CO may be used in a combustion heat recovery boiler.

[0006] A problem associated with full burn regenerators is the incomplete combustion of the dilute phase gas CO to CO<sub>2</sub>. The analogous problem with partial burn regenerators is incomplete consumption of O<sub>2</sub> in the dilute phase. Either problem gives rise to afterburning (CO combustion) in the cyclones, plenum, and flue gas transfer lines. The afterburning is exothermic, and the flue gas must absorb the heat of combustion, which decreases the amount of heat transferred to the catalyst bed.

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20 The maximum increase in the temperature allowed for the flue gas is generally governed by the temperature limits imposed by the materials of construction for the cyclones, plenum, and flue gas transfer lines. These limits require operators to maintain the catalyst bed at a lower temperature than desired to account for afterburning. The lower temperature in the catalyst bed ultimately limits the

25 throughput to the FCCU.

[0007] A need exists for a process and/or apparatus to control afterburning in the dilute phase zone of the regenerator without reducing the throughput of the FCCU.

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## SUMMARY

**[0008]** One embodiment of the present invention comprises a process for controlling afterburn in a catalyst regenerator of a fluidized catalytic cracking unit.

The regenerator comprises a catalyst bed and a dilute phase. The dilute phase is above the catalyst bed and below the inlets to the solid-gas separators. The dilute phase comprises (a) a first zone comprising oxygen (along with gases arising from the combustion of the coke on the spent catalyst and inert gases such as nitrogen from the air), wherein combustion in the first zone is fuel-limited; and (b) a second zone comprising carbon monoxide, wherein combustion in the second zone is

10 oxygen-limited. The process comprises the step of injecting an effective amount of steam into said dilute phase to substantially mixing the gases from the first zone and the second zone so that a substantial portion of the carbon monoxide combusts before passing through the inlet to the solid-gas separator.

**[0009]** Another embodiment of the present invention comprises a process for regenerating spent catalyst from the reaction zone of a fluid catalytic cracking reactor and comprises the steps of: (a) passing spent catalyst from the reaction zone of a fluid catalytic cracking reactor to a regenerator wherein the regenerator has therein a fluidized catalyst bed and a dilute phase zone above the catalyst bed,

20 wherein the dilute phase zone comprises the gases carbon monoxide and oxygen; (b) contacting the spent catalyst with a gas comprising oxygen to produce a regenerated catalyst; (c) passing the regenerated catalyst to the reaction zone; and, (d) mixing the gases present in the dilute phase zone by the injection of steam so that a substantial portion of the carbon monoxide present in the dilute phase zone 25 combusts.

**[0010]** Another embodiment of the present invention comprises: in a fluid catalytic cracking unit, a catalyst regenerator comprising: (a) a vessel having a fluidized catalyst bed therein with a dilute phase zone positioned above the catalyst

bed, wherein the dilute phase zone comprises (i) a first zone comprising carbon monoxide and oxygen, wherein combustion in the first zone is fuel-limited; (ii) a second zone comprising carbon monoxide and oxygen, wherein combustion in the second zone is oxygen-limited; and, (b) at least one steam inlet positioned to inject 5 steam into the dilute phase zone of the vessel to substantially mix the gases of the first and second zones without substantially disturbing the catalyst bed.

**[0011]** Another embodiment of the present invention comprises a regenerator for use in conjunction with a fluid catalytic cracking unit comprising a vessel 10 configured to have: (a) at least one internal bed section positioned near the lower end of the vessel, wherein the internal bed section is configured to hold a bed of catalyst; (b) a gas inlet positioned to allow an oxygen-containing gas to contact the bed of catalyst positioned within the vessel; (c) a spent catalyst inlet; (d) a regenerated catalyst outlet; (e) a flue gas outlet; (f) at least one solid-gas separator 15 having an inlet disposed within the vessel, wherein the separator inlet is positioned above the internal bed section; and, (g) at least one steam inlet positioned between the internal bed section and the separator inlet, the steam inlet configured to inject an effective amount of steam at a rate sufficient to substantially mix gases present in the area between the internal bed section and the separator inlet without substantially disturbing the catalyst bed positioned in the internal bed section while 20 the regenerator is in operation.

**[0012]** Another embodiment of the present invention comprises a process for regenerating spent catalyst from the reaction zone of a fluid catalytic cracking 25 reactor comprising the steps of: (a) passing spent catalyst from the reaction zone of a fluid catalytic cracking reactor to a regenerator, the regenerator having therein a fluidized catalyst bed and a dilute phase zone above the catalyst bed, the dilute phase zone comprising the gases carbon monoxide and oxygen; the dilute phase zone comprising a zone wherein carbon monoxide combustion is oxygen limited;

(b) contacting the spent catalyst with a gas comprising oxygen to produce a regenerated catalyst; (c) passing the regenerated catalyst to the reaction zone; and, (d) passing steam and an oxygen containing gas, preferably air, into the zone wherein carbon monoxide combustion is oxygen limited at a rate sufficient to 5 combust a substantial portion of the carbon monoxide present in the zone wherein carbon monoxide combustion is oxygen limited.

**[0013]** Another embodiment of the present invention comprises a process for regenerating spent catalyst from the reaction zone of a fluid catalytic cracking reactor in a regenerator comprising the steps of (a) passing spent catalyst from the reaction zone of a fluid catalytic cracking reactor to a regenerator operating under partial burn conditions, the regenerator having therein a fluidized catalyst bed and a dilute phase zone above the catalyst bed, the dilute phase zone comprising the gases carbon monoxide and oxygen; (b) contacting the spent catalyst with a gas comprising oxygen to produce a regenerated catalyst; (c) passing the regenerated catalyst to the reaction zone; and, (d) injecting steam into said dilute phase to cause mixing of the gases present in the dilute phase zone so that substantially all of the oxygen present in the dilute phase is depleted by combustion with carbon monoxide.

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**[0014]** Another embodiment of the present invention comprises a process for controlling afterburn in a catalyst regenerator of a fluidized catalytic cracking unit, the regenerator adapted to operate under partial burn conditions, the regenerator comprising a catalyst bed and a dilute phase, the dilute phase positioned above the catalyst bed and below an inlet to a solid-gas separator, the dilute phase comprising 25 (a) a first zone comprising oxygen, wherein combustion in the first zone is fuel-limited; (b) a second zone comprising carbon monoxide, wherein combustion in the second zone is oxygen-limited, the process comprising the step of substantially mixing the gases from the first zone and the second zone by the injection of an

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effective amount of steam so that a substantial portion of the oxygen present in the dilute phase reacts with carbon monoxide before passing through the inlet to the solid-gas separator.

5      **BRIEF DESCRIPTION OF THE DRAWINGS**

[0015]    Figure 1 illustrates an embodiment of a FCCU regenerator.

[0016]    Figure 2 illustrates the embodiment shown in Figure 1 with the dilute phase divided into zones.

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**DETAILED DESCRIPTION OF THE INVENTION**

[0017]    A maldistribution of CO and oxygen (O<sub>2</sub>) can exist in the dilute phase of the FCCU regenerator. For example, viewing Figure 1, (i) CO combustion above/near the spent catalyst inlet 110 is oxygen-limited, meaning that there may be an excess of fuel (CO) in the dilute phase 134 above the spent catalyst inlet 110; and (ii) CO combustion above the regenerated catalyst outlet 120/weir 121 in the dilute phase 134 is fuel (CO) limited, meaning there is an excess of O<sub>2</sub> in the zone above the regenerated catalyst outlet weir 121 in the dilute phase 134. When this maldistribution of gases are eventually mixed in the cyclones 154, 155, 156, plenum 158, and flue gas transfer line(s) 160, afterburning occurs because the uncombusted CO reacts with the O<sub>2</sub> to cause afterburning. The afterburning occurs because the CO and O<sub>2</sub> concentrations are no longer limiting factors.

[0018]    By mixing the dilute phase gases from the zones positioned above the spent catalyst inlet 110 and above the regenerated catalyst outlet 120/weir 121 before the gases reach the cyclones, afterburning in the cyclones 154, 155, 156, plenum 158, and flue gas transfer line(s) 160 decreases, thus allowing more heat absorption by the dense catalyst bed 130 and greater throughput to the FCCU. A

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similar effect is achieved by injecting an oxygen-containing gas into the dilute phase **134** where combustion is oxygen-limited.

[0019] FCCU feeds typically include hydrocarbonaceous oils boiling in the 5 range of about 430°F to about 1050°F (480-565°C), such as gas oil, heavy hydrocarbon oils comprising materials boiling above 1050°F (565°C); heavy and reduced petroleum crude oil; petroleum atmospheric distillation bottoms; petroleum vacuum distillation bottoms; pitch, asphalt, bitumen, other heavy hydrocarbon residues; tar sand oils; shale oil; liquid products derived from coal liquefaction 10 processes; and mixtures thereof. The FCC process of the present invention may be carried out in any type of fluid catalytic cracking unit without limitations as to the special arrangement of the reaction, stripping, and regeneration zones, etc. In general, the present invention can be used with conventional FCC processes and units regardless of the catalyst circulated in the FCCU. Typical catalysts used in 15 FCC operations include large-pore zeolites, such as zeolite Y.

[0020] The FCC feed passes to a FCCU where it is injected into the reaction zone and contacts a catalyst. The hot catalyst vaporizes and cracks the FCC feed at a temperature from about 450°C to about 650°C, preferably from about 500°C to 20 about 600°C to form cracked products. The cracking reaction deposits coke on the catalyst, thereby deactivating the catalyst or reducing the catalytic activity. The cracked products may be separated from the coked catalyst and at least a portion of the cracked products may be conducted to a fractionator and on to further processing.

[0021] The coked catalyst passes into a stripping zone where a stripping agent, such as steam, strips volatiles (strippable hydrocarbons) from the catalyst particles. The stripping may be performed under low severity conditions in order to retain adsorbed hydrocarbons on the catalyst for heat balance. The stripped catalyst passes to the regeneration zone **126** where it is regenerated by burning coke on the 25

catalyst in the presence of an oxygen-containing gas, preferably air. Decoking restores catalyst activity and simultaneously heats the catalyst to between 650°C and 800°C. The hot catalyst is then recycled to the FCC reaction zone.

[0022] Regeneration zone **126** comprises a large cylindrical regeneration vessel

5      **127** wherein the spent catalyst is maintained as a fluidized bed by passing an oxygen-containing regeneration gas, preferably air, up through the catalyst bed **130** via line **136** and distributor grid **138**. The fluidized catalyst forms a dense phase, or catalyst bed **130**, in the lower portion of the vessel **127** and a dilute phase **134** comprising entrained catalyst particles and gas between the upper level **132** of the catalyst bed **130** and the plenum **158** or the cyclone inlets **161**. The catalyst contacts the oxygen-containing regeneration gas under conditions sufficient to burn at least a portion, preferably a major portion, of the coke from the catalyst. Spent regeneration gas and entrained catalyst pass via one or more solid gas separators **154** (a primary cyclone **155** and a secondary cyclone **156**) before being recovered in the flue gas line **160** for disposal. The cyclones **155**, **156** separate entrained catalyst particles and return them to the bed **130** via cyclone diplegs **157** to prevent excessive losses of the entrained catalyst particles. The flue gas passes into a plenum chamber **158** prior to discharge from the regeneration zone **126** through line **160**. The regenerated catalyst is subsequently recycled to the reaction zone.

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[0023] In the embodiment shown in Figure 1, the regeneration zone is a vessel configured to have an internal bed section that holds the catalyst bed **130** during regeneration. The internal bed section is defined as the area below the top of the weir **121** of the regenerated catalyst outlet pipe **120**, and preferably between the top 25 of weir **121** and grid **138**. The regeneration zone **126** is preferably in a separate vessel containing a dense phase catalyst bed **130** in the internal bed section and having a level indicated at **132** (indicated also by the upper end of weir **121**) above that is a dilute phase **134**. In other embodiments not shown, the regeneration zone **126** may be configured as part of the same vessel as the FCCU reactor. The

catalyst in the dense phase catalyst bed **130** undergoes regeneration to burn off coke deposits formed in the reaction zone during the cracking reaction. An oxygen-containing regeneration gas enters the lower portion of regeneration zone **126** via line **136** and passes up through a grid **138** and the dense phase catalyst bed **130**, maintaining bed **130** in a fluidized condition.

[0024] Oxygen-containing regeneration gases used in the process of the present invention are those gases that contain molecular oxygen that may be mixed with an inert diluent gas. Air is a particularly suitable regeneration gas. Alternatively, air enriched with oxygen may be employed. Additionally, if desired, steam may be added to the dense phase bed **130** along with the regeneration gas or separately therefrom to provide additional inert diluents and/or fluidization gas.

[0025] The dilute phase **134** above the catalyst bed **130** comprises entrained catalyst particles, oxygen, and carbon monoxide (along with gases arising from the combustion of the coke on the spent catalyst and inert gases such as nitrogen from the air). Viewing Figure 2, in the embodiments of the present invention, the dilute phase **134** may be divided vertically (though not physically, see dotted line in Figure 2) into a first zone **I** and a second zone **II** that may or may not overlap. Zone **I** is preferably located above the overflow weir **121**, or entrance, to the regenerated catalyst outlet line **120**, and zone **II** is preferably located above the spent catalyst inlet line **110**. Carbon monoxide combustion above the spent catalyst inlet line **110** is  $O_2$  limited, meaning that there is an excess of fuel (CO) in zone **II** above the spent catalyst inlet line **110**. Carbon monoxide combustion above the regenerated catalyst outlet weir **121** is fuel (CO) limited, meaning there is an excess of  $O_2$  in zone **I** above the regenerate catalyst outlet weir **121**.

[0026] One or more steam inlets **200** or injectors **200** are positioned to inject, or pass, steam either alone or with the addition of an oxygen-containing gas into the

dilute phase **134** above the internal bed section and the catalyst bed **130**. The additional oxygen-containing gas can be injected into the dilute phase either separately or mixed with steam to enhance the combustion of CO to CO<sub>2</sub>. The preferred oxygen-containing gas is air. The steam and optionally oxygen-containing gas, preferably passes from a suitable source external from the unit. An effective amount of steam is injected at a rate to sufficiently mix the gas in zone **I** and the gas in zone **II** to promote substantial combustion of CO to CO<sub>2</sub>.

[0027] As used herein, injection of steam/oxygen-containing gas may also include flashing a liquid into the dilute phase **134** so the flashed liquid (now in vapor phase) performs the same function as injection of steam. This may or may not be desirable because of the energy (heat) requirements needed for flashing.

[0028] Alternatively, steam inlet **200** may be positioned to inject steam with or without an oxygen-containing gas only to the oxygen-limited zone (zone **II** in Figure 2). In embodiments where an oxygen-containing gas is injected into the oxygen-limited zone, the oxygen-containing gas passes into the oxygen-limited zone at a rate sufficient to promote substantially complete combustion of the CO in the oxygen-limited zone. In such embodiments, the oxygen-containing gas may or may not be injected at a rate sufficient to substantially mix zones **I** and **II** as long as combustion of CO is substantially complete as discussed below. These embodiments may be desirable for full-burn units where excess oxygen in the flue gas is acceptable; however, these embodiments may not be advantageous in partial-burn units where oxygen-depletion is desired.

[0029] In full-burn regenerators there is typically enough oxygen supplied to provide substantially complete combustion of CO and have excess oxygen (usually about 0.5 to 3 mole %) remaining in the flue gas. In partial-burn regenerators, there is not enough oxygen supplied to the unit to completely combust the CO, resulting

in 2 to 10 mole % CO passing with the flue gas after substantially all of the oxygen has been depleted. In either full- or partial-burn units, it is possible to have a maldistribution of dilute phase gases, resulting in the conditions in zones **I** and **II** as previously described. Either unit will benefit from mixing in the dilute phase **134** 5 to enhance combustion in the dilute phase **134** because most of the heat capacity of the dilute phase **134** is in the entrained catalyst that will carry the heat of combustion back to the dense bed **130**.

[0030] In a full-burn unit, the steam is preferably injected at a rate to sufficiently mix the gas in zone **I** and the gas in zone **II** to promote substantially complete combustion of CO to CO<sub>2</sub>, preferably at least 50 mole % combustion of CO to CO<sub>2</sub>, more preferably greater than 90 mole % combustion of CO to CO<sub>2</sub>, and most preferably substantially complete (>99 mole %) combustion of CO to CO<sub>2</sub>. At least 0.01 mole %, more preferably at least 0.5 mole % excess O<sub>2</sub> may remain in the 10 combustion product gas. These same conditions hold true for full-burn units wherein an oxygen-containing gas is injected only into the zone wherein combustion is oxygen-limited (zone **II** in Figure 2).

[0031] In a partial-burn unit, the steam is injected at a rate to sufficiently mix the gas in zone **I** and the gas in zone **II** to promote substantially complete consumption/depletion of O<sub>2</sub>, preferably at least 50 mole % depletion of O<sub>2</sub>, more preferably greater than 90 mole % depletion of O<sub>2</sub>, and most preferably substantially complete (> 99 mole %) depletion of all free O<sub>2</sub>. At least 0.5 mole %, more preferably at least about 2 mole %, and more preferably about 2 to about 10 15 mole %, excess CO may remain in the combustion product gas.

[0032] The steam is preferably injected radially inward at a location far enough above the catalyst bed **130** so that the injection of the steam will not disturb the catalyst bed **130** and cause additional catalyst to enter the dilute phase **134**. The

inlets **200** are positioned between the upper level **132** of the catalyst bed (above weir **121**) and the dilute phase inlets **161** to the primary cyclone(s) **155**. Preferably, the inlets **200** are located at least three feet above the upper level **132** of the catalyst bed **130**, and more preferably between three and nine feet above the upper level  
5 **132** of the catalyst bed **130**. When two or more injectors are used, they may or may not be positioned at the same height above the catalyst bed **130**. This positioning of the injectors allows most of the heat of combustion to preferably be imparted to the entrained solids in the dilute phase **134** that will eventually carry this heat back to the catalyst bed **130**. The injectors are preferably positioned to inject the steam  
10 substantially radially inward, though other configurations, such as tangential injection or combinations of injector configurations, may also be used, consistent with the objectives of substantially mixing the dilute phase **134** to promote CO combustion. For example, tangential injection may be preferred when the spent catalyst enters the regenerator tangentially. The choice of injector configuration(s)  
15 is within the skill of one of ordinary skill in the art and may depend on the dilute phase flow characteristics observed in a particular unit. It may also be desirable angle the injectors slightly upward to minimize the possibility of disturbing the catalyst bed. The velocity of the steam exiting the injectors is preferably subsonic, more preferably between 100 and 700 feet per second, and even more preferably  
20 between 300 and 500 feet per second.

[0033] The rate of steam passed to the dilute phase **134** can be adjusted online, as required, to meet the operating objectives of the unit. To control the rate of steam, the operator will monitor the maximum temperature in the cyclone outlets and the plenum **158**, relative to the temperature of the dense bed **130**, and will  
25 adjust the flow rate of steam to moderate the maximum temperature to less than 90°F (50°C) higher than the dense bed temperature, preferably to less than 45°F (25°C) above the dense bed temperature, more preferably to less than 18°F (10°C) and most preferably to less than 9°F (5°C) above the dense bed temperature.

[0034] The construction of the regeneration zone equipment described herein can be made with any material sufficiently able to withstand the relatively high temperatures involved if afterburning is encountered within the vessel and the high attrition conditions that are inherent in systems wherein fluidized catalyst is regenerated and transported. Various items such as valves, pumps, compressors, steam lines, instrumentation and other process equipment and control means have been omitted from the Figures for the sake of simplicity.

[0035] While the invention has been described in connection with specific embodiments, it will be understood that this invention is capable of modification, and that this application is intended to cover any variations, uses, or adaptations of the invention, including such departures from the present disclosure as come within known or customary practice in the art to which the invention pertains.

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